

discharge of energy which produces the large current flow will be accompanied by a release of heat. This energy is not entirely lost in that the consequent heating of the electrolyte solution increases the mobility of the ions which tends to increase the rate of electrolysis.

The configuration of the anode and cathode arrangement of electrolytic cell 41 is of significant importance. The fluted external periphery of the anode causes a concentration of current flow which produces a better gas yield over a given electrode area. This particular configuration also causes the surface area of the anode to be extended and permits an arrangement in which the anode and cathode have equal surface areas which is most desirable in order to minimize electrical losses. It is also desirable that the anode and cathode surfaces at which gas is produced be roughened, for example by sand-blasting. This promotes separation of the gas bubbles from the electrode surfaces and avoids the possibility of overvoltages.

The arrangement of the secondary transformer in which the central anode is surrounded by the cathode is also of great importance. The anode, being constructed of a magnetic material, is acted on by the magnetic field of transformer TR2 to become, during the period of energization of that transformer, a strong conductor of magnetic flux. This in turn creates a strong magnetic field in the interelectrode space between the anode and the cathode. It is believed that this magnetic field increases the mobility of the ions in solution thereby improving the efficiency of the cell.

The heat generated by transformer TR2 is conducted via the anode to the electrolyte solution and increases the mobility of the ions within the electrolyte solution as above mentioned. The cooling fins 180 are provided on casing 171 to assist in dissipation of excess generated heat. The location of the transformer within the anode also enables the connections of the secondary coil 89 to the anode and cathode to be made of short, well protected conductors.

As mentioned above the hydrogen and oxygen gas generated in electrolytic cell 41 and collected in ducts 244, 251 is delivered to a gas mixing chamber of the mixing and delivery unit 38. More specifically, these gases are delivered from ducts 244, 251 via escape valves 283, 284 (FIG. 15) which are held in position over discharge ports 285, 286 from the ducts by means of a leaf spring 287. The outer ends of spring 287 engage the valves 283, 284 and the centre part of the spring is bowed inwardly by a clamping stud 288 screwed into a tapped hole in a boss 289 formed in the cell casing 171.

Valve 283 is detailed in FIGS. 28 and 29 and valve 284 is of identical construction. Valve 283 includes an inner valve body 291 having a cap portion 292 and an annular end ring portion 293 which holds an annular valve seat 294. A valve disc 295 is biased against the valve seat by a valve spring 296 reacting against the cap portion 292. An outer valve cover 297 fits around the inner member 291 and is engaged by spring 287 to force the inner member firmly into a socket in the wall of the cell casing so to cover the hydrogen discharge port 285. The end ring portion 293 of the inner body member beds on a gasket 298 within the socket.

During normal operation of the apparatus valves 283, 284 act as simple one-way valves by movements of their spring loaded valve plates. However, if an excessive gas pressure should arise within the electrolytic cell these valves will be forced back against the action

of holding spring 287 to provide pressure relief. The escaping excess gas then flows to atmosphere via the mixing and delivery unit 38 as described below. The pressure at which valves 283, 284 will lift away to provide pressure relief may be adjusted by appropriate setting of stud 288, which setting is held by a nut 299.

The construction of the gas mixing and delivery unit 38 is shown in FIGS. 30 and 40. It comprises an upper body portion 301 which carries an air filter assembly 302, an intermediate body portion 303, which is bolted to the casing of electrolytic cell 41 by six studs 304, and successive lower body portions 305, 300, the latter of which is bolted to the inlet manifold of the engine by four studs 306.

The bolted connection between intermediate body portion 303 and the casing of the electrolytic cell is sealed by a gasket 307. This connection surrounds valves 283, 284 which deliver hydrogen and oxygen gases directly into a mixing chamber 308 (FIG. 34) defined by body portion 303. The gases are allowed to mix together within this chamber and the resulting hydrogen and oxygen mixture passes along small diameter horizontal passageway 309 within body portion 303 which passageway is traversed by a rotary valve member 311. Valve member 311 is conically tapered and is held within a correspondingly tapered valve housing by a spring 312 (FIG. 38) reacting against a bush 313 which is screwed into body portion 303 and serves as a mounting for the rotary valve stem 314. Valve member 311 has a diametral valve port 315 and can be rotated to vary the extent to which this port is aligned with passageway 309 thereby to vary the effective cross-section for flow through that passageway. As will be explained below, the rotational positions of the valve member is controlled in relation to the engine speed.

Passage 309 extends to the lower end of a larger diameter vertical passageway 316 which extends upwardly to a solenoid freed valve 310 incorporated in a valve and jet assembly denoted generally as 317.

Assembly 317 comprises a main body 321 (FIG. 32) closed at the top by a cap 322 when the assembly is clamped to body portion 303 by two clamping studs 323 to form a gas chamber 324 from which gas is to be drawn through jet nozzles 318 into two vertical bores or throats 319 (FIG. 31) in body portion 303. The underside of body 321 has a tapped opening into which is fitted an externally screw threaded valve seat 325 of valve 310. A valve member 326 is biased downwardly against seat 325 by a spring 327 which reacts against cap 322. Spring 327 encircles a cylindrical stem 328 of valve member 326 which stem projects upwardly through an opening in cap 322 so that it may be acted on by solenoid 56 which is mounted immediately above the valve in upper body portion 301.

Solenoid 56 is comprised of an outer insulating casing 366 which has two mounting flanges 367. This casing houses the copper windings constituting coil 55. These are wound on a plastic bobbin 369 disposed about a central mild steel core 371. The core has a bottom flange 372 and the bobbin and coils are held clamped in the casing through insulating closure 373 acted on by flange 372 on tightening of a clamping nut 374 which is fitted to the other end of the core.

Upper body portion 301 of unit 38 is tubular but at one side it has an internal face shaped to suit the exterior profile of solenoid casing 366 and mounting flanges 367. Two mounting screws 375 screw into holes